

Preparation of the New Low-Cost K_2CO_3/Al_2O_3 Sorbent for CO_2 Capture at Flue Gas Operating Conditions

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Abstract: In this study, the preparation of the new low-cost potassium carbonate on alumina support sorbents prepared by impregnating K_2CO_3 on industrial grade of Al_2O_3 support was investigated. The CO_2 capture capacity was measured in the presence of H_2O in a fixed-bed reactor at CO_2 capture temperature of $60^\circ C$ using breakthrough curves. The sorbent developed showed the adsorption capacity of $75.4 \text{ mgCO}_2/\text{g}$ sorbent. The stability of sorbent capture capacity is higher than the reference sorbent. The changes in the pore volume and surface area are $0.020 \text{ cm}^3/\text{g}$ and $5.5 \text{ m}^2/\text{g}$, respectively after 5 cycles adsorption and regeneration. The small changes occur in the pore size distribution and surface area of sorbent after 5 cycles. This sorbent can be considered for large-scale applications.

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1. Introduction:

Global warming increasingly thought to be associated with the atmospheric emission of greenhouse gases. Carbon Dioxide is a major greenhouse gas that is released into the atmosphere due to the use of fossil fuels. Large amounts of CO_2 are emitted in diluted streams at atmospheric pressure, for instance, in flue gases from power stations, as the fuel is usually burned in air. It can be removed from these streams by various methods such as membrane separation, amine scrubbing, and using molecular sieves [1-3]. These methods however are costly and energy intensive.

Solid sorbent processes for CO_2 capture are also under study. The use of solid sorbents can be a highly cost-effective and energy efficient way to remove CO_2 [4-7]. Sorbents containing alkali and alkaline-earth metals like potassium carbonate and calcium oxide are investigated for this commercial feasibility [8].

Alkaline-earth method-based sorbents such as MgO and CaO are applicable at much higher adsorption and regeneration temperatures [7]. Alkali metal-based sorbents were employed in CO_2 adsorption at low temperatures ($50-70^\circ C$) with thermal regeneration easily occurring at low temperatures ($<200^\circ C$). CO_2 capture using a dry sodium-based sorbent was also reported [9,10]. However, when CO_2 reacted with Na_2CO_3 , the global carbonation reaction rate was rather slow [11]. The CO_2 adsorption and regeneration of potassium-based sorbents with several supports such as activated carbon [4,5,12], TiO_2 , SiO_2 , MgO , ZrO_2 , CaO and Al_2O_3 were studied [6,9,13,14]. Al_2O_3 is one of the most proper materials used as sorbent support. An

Ideal dry sorbent must have a high CO_2 capture capacity, high adsorption rate, excellent regeneration property, and high attrition resistance to remove CO_2 from the flue gas.

In all of the previous works, initial materials used were from high pure materials that have low impurities and high costs. The objective of this work is to develop a low-cost, high-capacity CO_2 sorbent and to demonstrate its technical and economical potentials for post-combustion CO_2 capture. For synthesis of this sorbent industrial grade of alumina (that has the highest cost in sorbent preparation) was used and some of the important specifications of the prepared sorbent such as, capture capacity at single and multiple cycles, surface area, and structural properties are obtained in this work.

2. Experimental

Preparation of Sorbents. The potassium-based sorbents used in this study were prepared by impregnating K_2CO_3 (Merck) on Alumina of industrial grades as support. Twenty (20.0) g of Al_2O_3 was added to 100 ml of an aqueous solution of anhydrous potassium carbonate with 9wt% concentration in deionized water. Then, it was mixed with a magnetic stirrer at room temperature for 24 hours. After that, the mixture was dried in a rotary vacuum evaporator at $60^\circ C$. The dried samples were calcined in a furnace under the N_2 flow (100 cc/min) for 4 hours at $300^\circ C$. The amount of K_2CO_3 loaded was 23.2% and the sorbent had an apparent density of 2.44 g/cm^3 .

Apparatus and Procedures. A fixed-bed Stainless-Steel reactor (diameter of 15 mm), which was placed in an electric furnace under atmospheric

pressure was used for adsorption process. Two (2.0) g of the sorbent was packed into the reactor. In order to prevent condensation of water vapor injected into the reactor and the GC column, the temperatures of the inlet and outlet lines of the reactor were maintained above 100 °C. The column used in this analysis was a 1/8 in. stainless tube packed with Porapak Q. When the CO₂ concentration of the outlet gas reached the same level as that of the inlet gas in the CO₂ adsorption process, process was stopped. The outlet gas from the reactor was automatically analyzed every 5 min by a thermal conductivity detector (TCD), which was equipped with an auto sampler (Valco online valve). Schematic diagram of the fixed-bed reactor is shown in Fig. 1.

The feed stream comprises of Nitrogen, carbon dioxide and water. The liquid water flow rate was controlled using a piston pump and the water

was vaporized before entering the column. Both CO₂ and N₂ flow rates were controlled by independent mass flow controllers and these gases were mixed with the vaporized water inside the oven where experiments were done. All the CO₂ sorption tests were performed following the same procedure.

The CO₂ capture capacity of the sorbent was evaluated by the breakthrough curve for CO₂ adsorption. In this study, the CO₂ capture capacity of sorbent was calculated from its breakthrough curve during CO₂ adsorption in the presence of 9.0 vol.% H₂O and 1 vol.% CO₂. The CO₂ capture capacity describes the amount of CO₂ absorbed until the output concentration of CO₂ reached 1 vol.%, which is the same value as that of the inlet. Adsorption and regeneration processes were carried out at 60 °C and 200 °C, respectively.

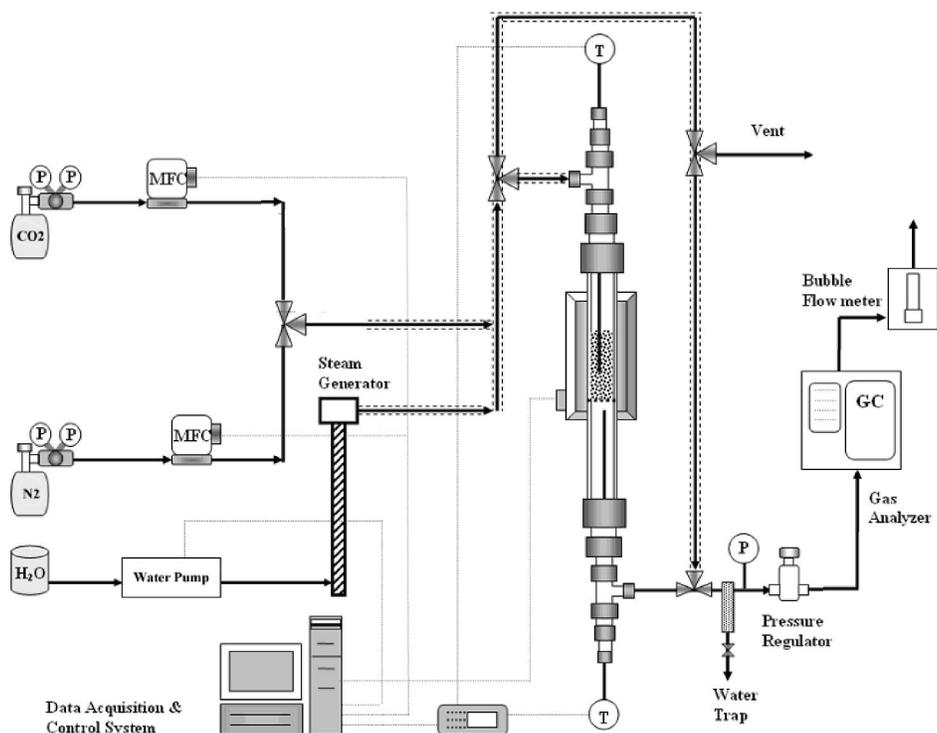


Fig 1. Schematic Diagram of the fixed-Bed Reactor

3. Results and Discussion

Fig. 2 shows the CO₂ Breakthrough Curve (CO₂ concentration changes during adsorption step at the bed outlet) for new developed sorbent. The CO₂ concentration was nearly zero for about first 10 min,

indicating that CO₂ was completely adsorbed. The CO₂ concentration then slowly increased to 1% after 180 min indicating the complete conversion of available K₂CO₃ in sorbent at this time.

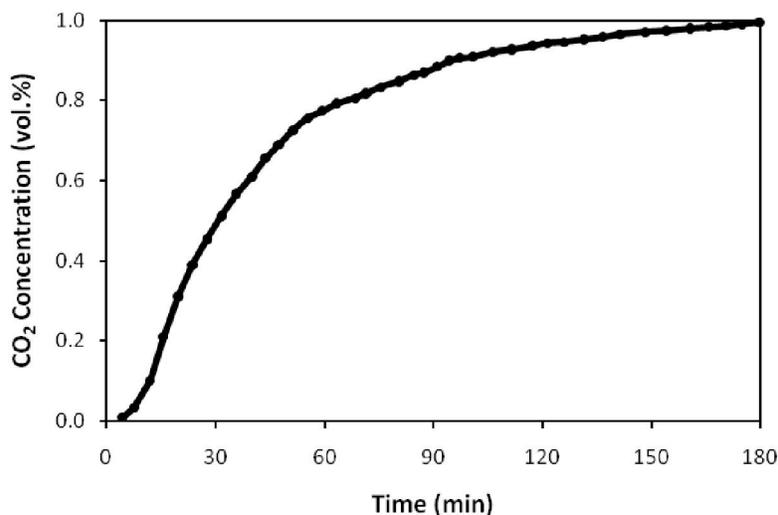


Fig 2. Change of the CO₂ Concentration during adsorption

Fig. 3 shows the total CO₂ capture capacities of the new low-cost sorbent as well as those obtained [15] as a function of cycle number. In this figure both adsorption and regeneration are considered as a one-cycle process. As shown in Fig. 3, the total capture capacity of the new low-cost sorbent was about 75.4 mg CO₂/g sorbent at the first cycle. This amount is lower than the value of the

reference sorbent at the first cycles; but the stability of capture capacity is higher because, after 5 cycles, capture capacity decreases by 35% that is lower than the reference sorbent. These results show that new low-cost sorbent developed in this study is more suitable for multiple cycle operations necessary for industrial applications.

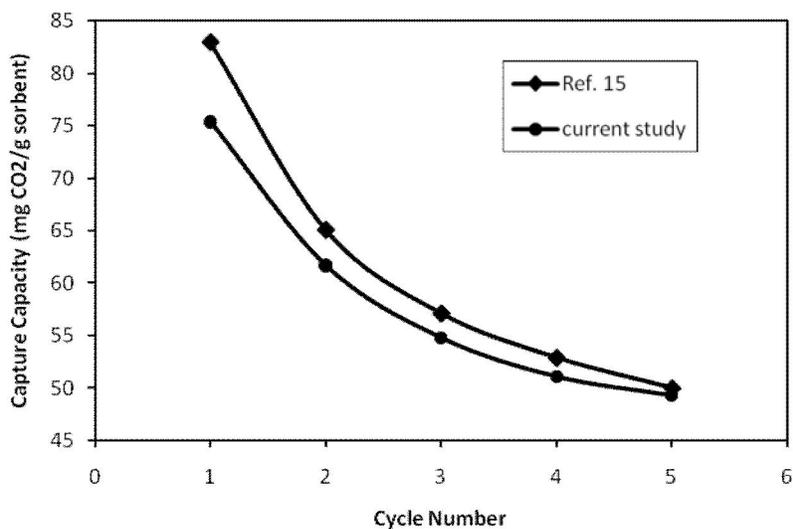


Fig 3. The CO₂ capture capacity of the sorbents as function of cycle number

For study on Sorbent structure change during adsorption and regeneration process three samples (0.5 g) were taken after the 1st, 3rd, and 5th cycles, respectively, and the surface area and pore volume were measured with N₂ adsorption method.

The pore volume and the surface area of the samples are shown in Fig. 4. The surface area and pore volume of sorbent decrease as the number of cycles increases.

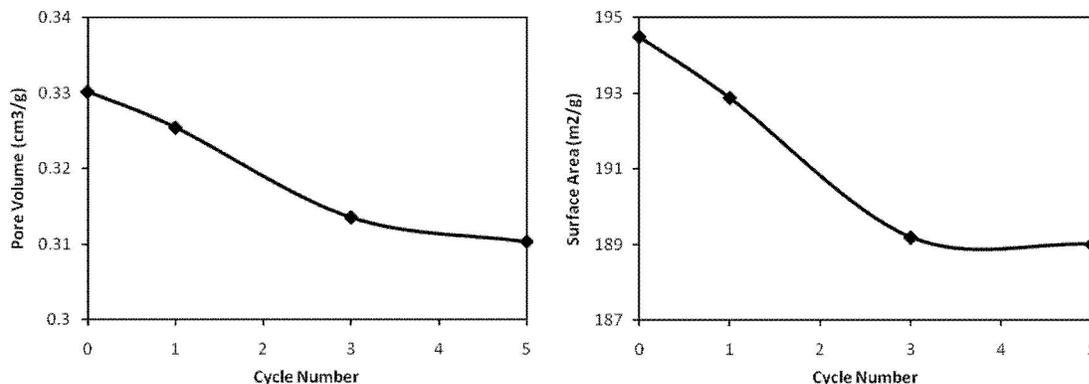


Fig 4. Changes of the pore volume and surface area with the cycle number

As shown in Fig. 5, for 80% of pores of the fresh sorbent, the pore size distribution range from 1.8 to 20.0 nm. The maximum value of the pore

volume appears at 5.4 nm. There is a little change in pore size distribution after 5 cycles.

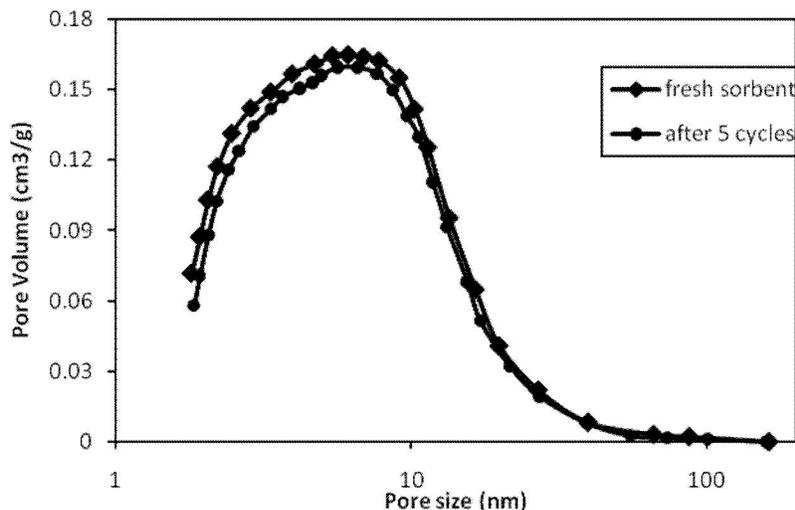


Fig 5. Pore size distribution of sorbent

The SEM images for fresh sorbent and sorbent after 5 cycles are shown in Fig. 6. The SEM

images confirm that the change in the structure is minimal after 5 cycles.

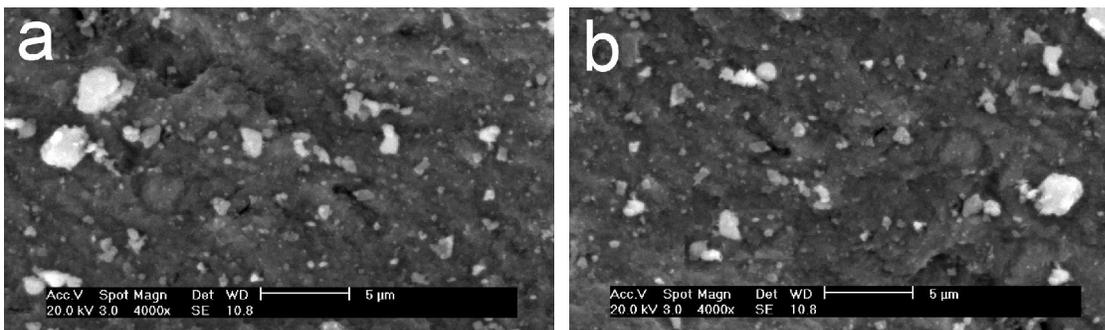


Fig 6. Scanning electron micrographs of sorbent: (a) fresh sorbent; (b) after 5 cycles

4. Conclusion

The low-cost sorbent developed in this study showed 75.4 mgCO₂/g sorbent in present of 1.0% CO₂ and 9.0 vol.% H₂O at 60°C. The capture capacity of sorbent as a function of cycle number was investigated in a fixed-bed reactor. The stability of sorbent capture capacity is higher than the reference sorbent. The changes in the pore volume and surface area are 0.020cm³/g and 5.5m²/g, respectively. Small changes occur in the pore size distribution and surface area of the prepared sorbent. This sorbent could be used for an industrial CO₂ capture processes with fixed-bed reactors. To investigate this purpose, a dual fixed-bed reactor is needed for operating at real cyclic steady-state condition.

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